

# Noninteracting Bosas of mass m & spins

(7)

$$\langle M_{\vec{h}, \sigma} \rangle = \frac{1}{e^{\beta(\epsilon_{\vec{h}} - \mu)} - 1} ; \quad \epsilon_{\vec{h}} = \frac{\hbar^2 \vec{h}^2}{2m}$$

$$-\infty < \mu < 0 \Leftrightarrow 0 < \beta < 1$$

## Occupation of energy levels

$$\begin{aligned} f_0 &= \underbrace{\frac{g}{\sqrt{v}} \frac{1}{e^{-\beta\mu_0}}}_{f_{GS} \text{ in ground state}} + \underbrace{\frac{g}{\sqrt{v}} \sum_{\vec{h} \neq 0} \frac{1}{e^{\beta[\epsilon(\vec{h}) - \mu_0]} - 1}}_{f_{ES} \text{ in excited states}} \\ &= \frac{g}{\sqrt{v}} \frac{\beta}{1 - \beta} + \frac{g}{\sqrt{v}} f_{\beta/2}^+(\beta) ; \quad f_m^+(\beta) = \frac{1}{(m-1)!} \int_0^\infty dx \frac{x^{m-1}}{\beta e^{-\beta x} - 1} \end{aligned}$$

$$\text{For } \beta < 1, \quad f_{ES}(\beta) < \frac{g}{\sqrt{v}} f_{\beta/2}^+(1) \equiv f_{ES}^{MAX} = 2.612 g^{-1/3}$$

## Canonical ensemble

$$f_0 = f_{GS}(\beta) + f_{ES}(\beta) \Rightarrow \text{eq}^0 \text{ for } \beta.$$

$$\text{If } f_0 < f_{ES}^{MAX}, \quad \beta < 1, \quad f_0 = \underbrace{f_{GS}(\beta)}_{\rightarrow 0} + f_{ES}(\beta) \xrightarrow[V \rightarrow \infty]{} f_{ES}(\beta)$$

$$\text{If } f_0 > f_{ES}^{MAX}, \quad \beta \rightarrow 1 \quad \& \quad f_{GS} = f_0 - f_{ES}^{MAX} \text{ finite.}$$

True Bose Einstein Condensation with a finite fraction  $\alpha = \frac{f_{GS}}{f_0}$  in the ground state.

$$\text{Then, } \langle n_0 \rangle = \alpha V \beta_0 = \frac{g}{\beta^{-1} - 1} \Rightarrow \beta^{-1} = 1 + \frac{g}{\alpha V \beta_0} \quad \& \quad \beta \approx 1 - \frac{g}{\alpha V \beta_0} \xrightarrow[V \rightarrow \infty]{} 1$$

Is  $n_0$  the sole macroscopically occupied state?

$$\langle n_i \rangle = \frac{1}{\beta^{-1} e^{\beta \epsilon_i} - 1} \quad ; \quad \epsilon_i = \frac{2\pi}{L} \Rightarrow \beta \epsilon_i = \beta \frac{\hbar^2}{2m} \frac{4\pi^2}{L^2} = \frac{k}{L^2}$$

$$\langle n_i \rangle = \left[ \left( 1 + \frac{g}{\alpha L^3 \beta_0} \right) \left( 1 + \frac{k}{L^2} \right) - 1 \right]^{-1} \approx \left[ \frac{k}{L^2} + \frac{1}{\alpha \beta_0 L^3} \right]^{-1} \xrightarrow{k} \frac{L^2}{k}$$

$$g_i = \frac{\langle n_i \rangle}{V} \approx \frac{1}{L} \xrightarrow[V \rightarrow \infty]{} 0$$

Only the ground state has a macroscopic number of particle

### Transition Temperature

$\mu$  or  $N$  are not the easiest control parameter, but we can

use  $\beta_{ES}^{MAX} = g \left( \frac{2\pi m k_B T}{\hbar^2} \right)^{3/2} f_{3/2}^+(1)$  by changing  $T$ .

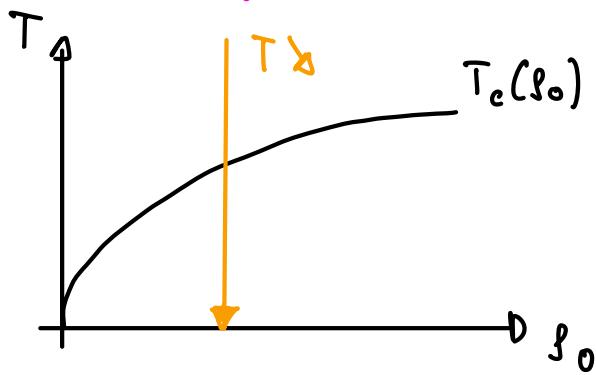
\*  $T > T_c$ ,  $\beta_{ES}^{MAX} > \beta_0$ ,  $\beta < 1$  &  $\beta_{GS} \xrightarrow[V \rightarrow \infty]{} 0 \Rightarrow$  No BEC

$$* T = T_c, \quad \beta_0 = \beta_{ES}^{MAX} \Rightarrow \boxed{\hbar_B T_c = \frac{\hbar^2}{2\pi m} \left( \frac{\beta_0}{g f_{3/2}^+(1)} \right)^{2/3}}$$

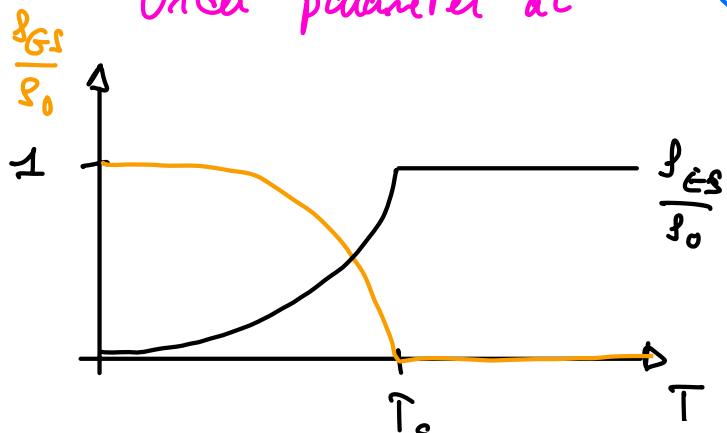
\*  $T < T_c$ ,  $\beta_{GS} = \beta_0 - \underbrace{\beta_{ES}^{MAX}(T)}_{\propto T^{3/2}}$ . Since  $\beta_0 = \beta_{ES}^{MAX}(T_c)$ , we have

$$\frac{\beta_{GS}}{\beta_0} = 1 - \left( \frac{T}{T_c} \right)^{3/2}$$

## Phase diagram



Order parameter at



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Comment: Why can we use  $\mathfrak{f}_0 = \mathfrak{f}_{GS}(\mathfrak{z}) + \mathfrak{f}_{ES}(\mathfrak{z})$  in the canonical ensemble while we derived it in the grand canonical ensemble?

[Grisenti, Salasnich, Sancilio, Zannetti, Arxiv: 2404.17300]

## Thermodynamics

Grand potential : Treating the GS separately

$$G = k_B T g \left[ \ln(1-\mathfrak{z}) + \frac{V}{(2\pi)^3} \int dh \frac{4\pi h^2}{m} \ln \left( 1 - \mathfrak{z} e^{-\beta \frac{h^2}{2m}} \right) \right]$$

$$x = \frac{\pi h^2}{2m k_B T} \Rightarrow h = \sqrt{x} \sqrt{\frac{8\pi^2 m k_B T}{h^2}}$$

$$G = k_B T g \ln(1-\mathfrak{z}) + \frac{g V k_B T}{4\pi^2} \left( \frac{8\pi^2 m k_B T}{h^2} \right)^{3/2} \int dx x^{1/2} \ln(1-\mathfrak{z} e^{-x})$$

$$\text{IBP} - \frac{2}{3} \int dx \frac{x^{3/2} \mathfrak{z} e^{-x}}{1 - \mathfrak{z} e^{-x}}$$

$$G = k_B T g \ln(1-\mathfrak{z}) - \frac{g V k_B T}{\pi^3} \underbrace{\frac{2}{3} \frac{2}{\sqrt{\pi}}}_{\frac{1}{3!}} \int dx \frac{x^{3/2}}{\mathfrak{z}^{-1} e^x - 1} \underbrace{\mathfrak{f}_{S_{12}}^+(\mathfrak{z})}_{}$$

$$G = \hbar_B T g \ln(1-\zeta) - \frac{g \hbar_B T}{\lambda^3} f_{S/2}^+(3)$$

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Pressure:  $P = -\frac{\partial G}{\partial V} = \frac{g \hbar_B T}{\lambda^3} f_{S/2}^+(3) \Rightarrow$  the FS bosons do not contribute to the pressure.

This makes sense:  $\vec{h}_0 = 0$  so that  $\vec{p}_0 = \vec{t} \cdot \vec{h}_0 = 0 \Rightarrow$  no momentum to transfer

$T < T_c$   $P = \frac{g \hbar_B T}{\lambda^3} f_{S/2}^+(1) \approx 1.31 \frac{g \hbar_B T}{\lambda^3} \Rightarrow$  independent from  $N & V$ !

$T > T_c$   $\xi_0 \approx \frac{g}{\lambda^3} f_{S/2}^+(3) \Rightarrow P = \xi_0 \hbar_B T \frac{f_{S/2}^+(3)}{f_{S/2}^+(1)}$

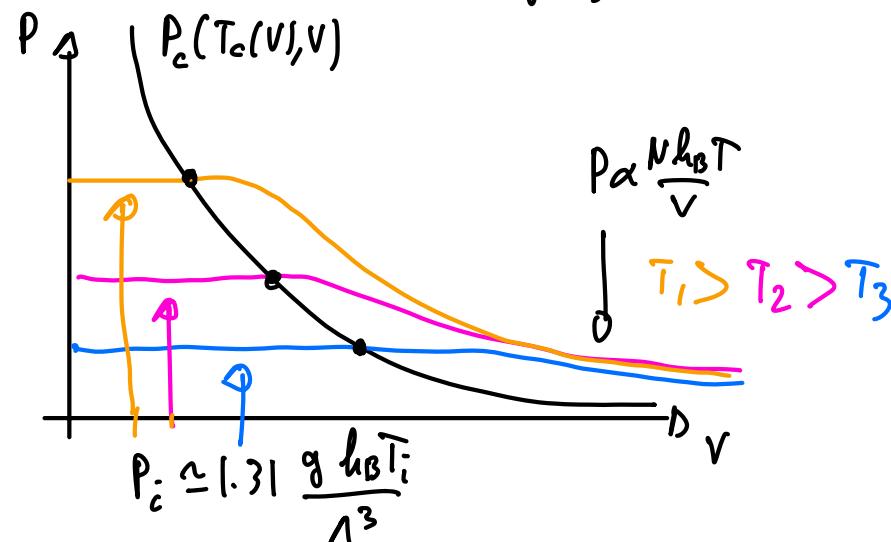
$$T \gg T_c ; \zeta \ll 1, f_m^+(\zeta) = \frac{1}{(m-1)!} \int_0^\infty dx \frac{x^{m-1}}{z^{-1} e^{x-1}} \approx \frac{z}{(m-1)!} \underbrace{\int_0^\infty dx x^{m-1} e^{-x}}_{(m-1)!}$$

$\Rightarrow P \rightarrow \xi_0 \hbar_B T$  as expected.

$T = T_c$   $\xi_0 = \frac{N}{V} = \frac{g f_{S/2}^+(1)}{\lambda^3} (2 \pi m \hbar_B T_c)^{3/2} \Rightarrow T_c(V) = \frac{1}{2 \pi m \hbar_B T_c} \left( \frac{N \lambda^3}{V g f_{S/2}^+(1)} \right)^{2/3}$

$$\Rightarrow \text{At } T_c, P_c(T_c(V), V) \propto \frac{N T_c(V)}{V} \sim \frac{1}{V \xi_0}$$

Isotherm  $P(V)$



High temperature expansion: how to connect to classical stat mech?

$f_m^+(z) \approx z \Rightarrow$  leading order term  $\Rightarrow$  what about higher orders?

$$f_m^+(z) = \sum_{k=1}^{\infty} \frac{z^k}{k^m} \approx z + \frac{z^2}{2^m} + \frac{z^3}{3^m} + \dots$$

$$f_m^+(z) = \frac{1}{(m-1)!} \int_0^{\infty} dx x^{m-1} z e^{-x} \sum_{k=0}^{\infty} (ze^{-x})^k = \frac{1}{(m-1)!} \sum_{k=0}^{\infty} z^{k+1} \int_0^{\infty} dx x^{m-1} e^{-x(1+k)}$$

$m = x(1+k)$

$\frac{(m-1)!}{(1+k)^m}$

From here  $\Rightarrow P$  as a series in  $z$       }       $\Rightarrow P$  as a series in  $\xi_0$ .  
 $\xi_0$  as a series in  $z$       }

Energy & heat capacity:

$$\langle E \rangle = \partial_{\beta} (\beta E) = \frac{3gV}{\lambda^4} f_{S_{1/2}}^+ (z) \frac{\partial \lambda}{\partial \beta} ; \lambda = \sqrt{\frac{\hbar^2 \beta}{8\pi m}} \Rightarrow \partial_{\beta} \lambda = \frac{\hbar_B T}{2} \lambda$$

$$\langle E \rangle = \frac{3}{2} \hbar_B T \frac{gV}{\lambda^3} f_{S_{1/2}}^+ (z) = \frac{3}{2} PV$$

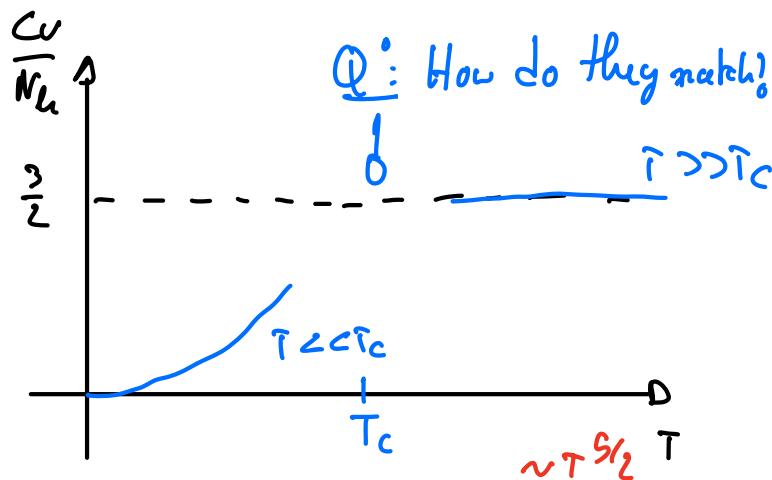
Low temperature limit

$$T > T_c, \xi_{GS} = 0 \quad \& \quad N \approx \frac{gV}{\lambda^3} f_{S_{1/2}}^+ (z) \Rightarrow E = \frac{3}{2} N \hbar_B T \frac{f_{S_{1/2}}^+ (z)}{f_{S_{1/2}}^+ (1)}$$

$T \gg T_c$  leads to  $E \approx \frac{3}{2} N \hbar_B T$  &  $C_V = \frac{3}{2} N$ .

$$T = T_c, \xi_0 = \frac{g}{\lambda_c^3} f_{S_{1/2}}^+ (1) \quad \& \quad gV = \frac{N \lambda_c^3}{f_{S_{1/2}}^+ (1)}$$

$$T < T_c, \langle E \rangle = \frac{3}{2} N \hbar_B T \left( \frac{\lambda_c}{\lambda} \right)^3 \frac{f_{S_{1/2}}^+ (1)}{f_{S_{1/2}}^+ (1)} \propto N T^{5/2} \Rightarrow C_V \propto T^{3/2} N$$



$$T > T_c ; \langle E \rangle = \frac{3}{2} h_B T \frac{gV}{\lambda^3} f_{1/2}^+(z)$$

$$C_V = \frac{3}{2} h_B T \frac{gV}{\lambda^3} \left[ \frac{5}{2T} f_{3/2}^+(z) + \underbrace{\frac{\partial z}{\partial T} \cdot \frac{\partial}{\partial z} f_{1/2}^+(z)}_{\textcircled{1}} \right]$$

$$\textcircled{1} \text{ Direct algebra } \frac{\partial z}{\partial T} f_m^+ = \frac{1}{z} f_{m-1}^+ = \frac{\partial}{\partial x} \left[ -\frac{1}{z^{-1} e^{x-1}} \right]$$

$$\frac{\partial}{\partial z} \int_0^\infty dx \frac{x^{m-1}}{z^{-1} e^{x-1}} = - \int_0^\infty dx \frac{x^{m-1}}{(z^{-1} e^{x-1})^2} \left( -\frac{1}{z}, e^x \right) = \frac{1}{z} \int_0^\infty dx \frac{z^{-1} e^x}{(z^{-1} e^{x-1})^2} x^{m-1}$$

$$\stackrel{\text{IBP}}{=} \frac{m-1}{z} \int_0^\infty dx \frac{x^{m-2}}{z^{-1} e^{x-1}}$$

Multiplying both sides by  $\frac{1}{m!}$  leads to  $\frac{\partial}{\partial z} f_m^+ = \frac{1}{z} f_{m-1}^+$

$$\textcircled{2} \quad z_0 \lambda^3 = g f_{1/2}^+(z) \Rightarrow \frac{\partial}{\partial T} \ln(z_0 \lambda^3) = -\frac{3}{2T} = \frac{2T f_{3/2}^+(z)}{f_{1/2}^+(z)} = \frac{1}{z} \frac{f_{1/2}^+(z)}{f_{1/2}^+(z)} \frac{\partial z}{\partial T}$$

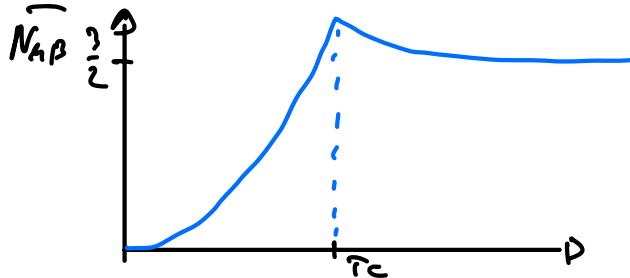
$$\Rightarrow \frac{\partial z}{\partial T} = -\frac{3z}{2T} \frac{f_{1/2}^+(z)}{f_{1/2}^+(z)}$$

① + ②  $\Rightarrow$ 

$$C_V = \frac{15}{4} k_B \frac{gV}{\lambda^3} f_{S_{1/2}}^+(z) - \frac{9}{4} k_B \frac{gV}{\lambda^3} \frac{f_{S_{1/2}}^+(z)^2}{f_{V_2}^+(z)}$$

$$\left. \begin{array}{l} \text{As } T \rightarrow T_C, \quad f_{S_{1/2}}^+ \rightarrow 1.34 \\ f_{S_{1/2}}^+ \rightarrow 9.61 \\ f_{V_2}^+ \rightarrow \infty \end{array} \right\}$$

$$C_V \rightarrow \frac{15}{4} k_B \frac{gV}{\lambda^3} f_{S_{1/2}}^+(1) \quad \text{&} \quad \frac{C_V}{Nk_B} \simeq 1.92 > \frac{3}{2}$$



High temperature expansion The approach to  $T = T_C$   
 $T > T_C$

arises on a high- $T$  expansion, which leads to  $\frac{C_V}{Nk_B} \simeq \frac{3}{2} \left( 1 + \beta_0 \frac{1}{2} \frac{1}{T} + \dots \right) \geq \frac{3}{2}$